

# Soil Science and Soil Physics

*Lecture 8*

**Water flow in soil,  
hydraulic conductivity**



# Saturated flow

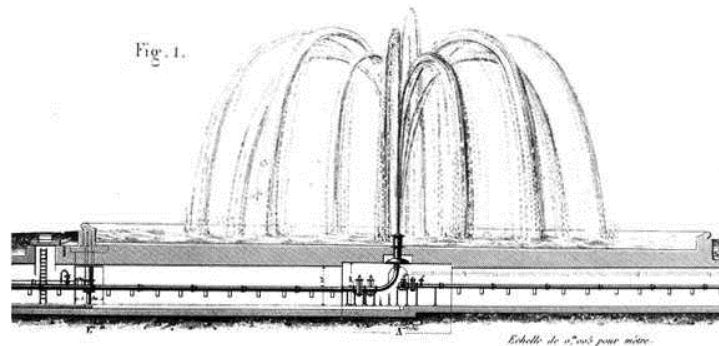
**Henry Darcy (1856)** filtration of water for fountains in Dijon

After many experiments he found that **water flow** through the soil column depends on:

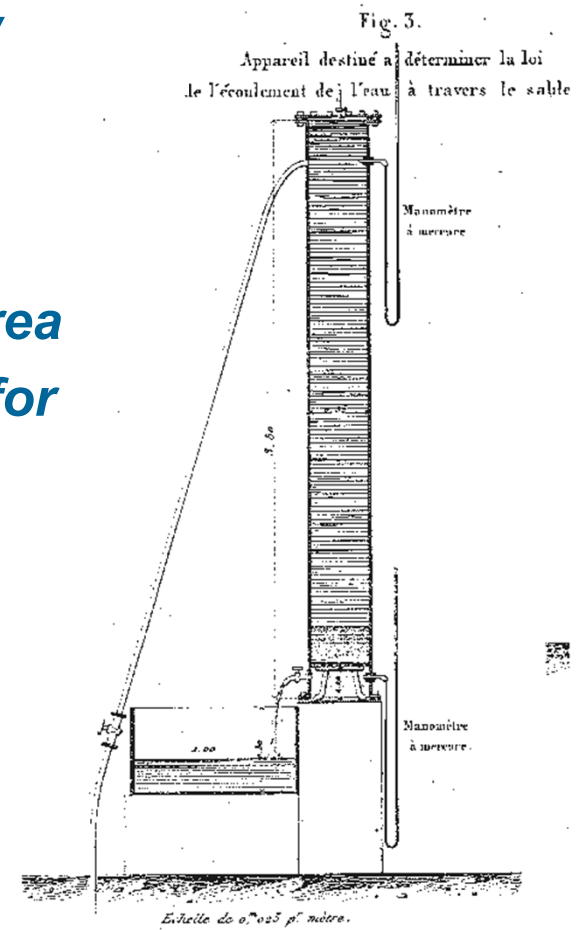
- **directly proportional to pressure drop**
- **inversely proportional to the length**
- **directly proportional to the crosssectional area**
- **dependent on coefficient which is specific for each media**



Henry Darcy

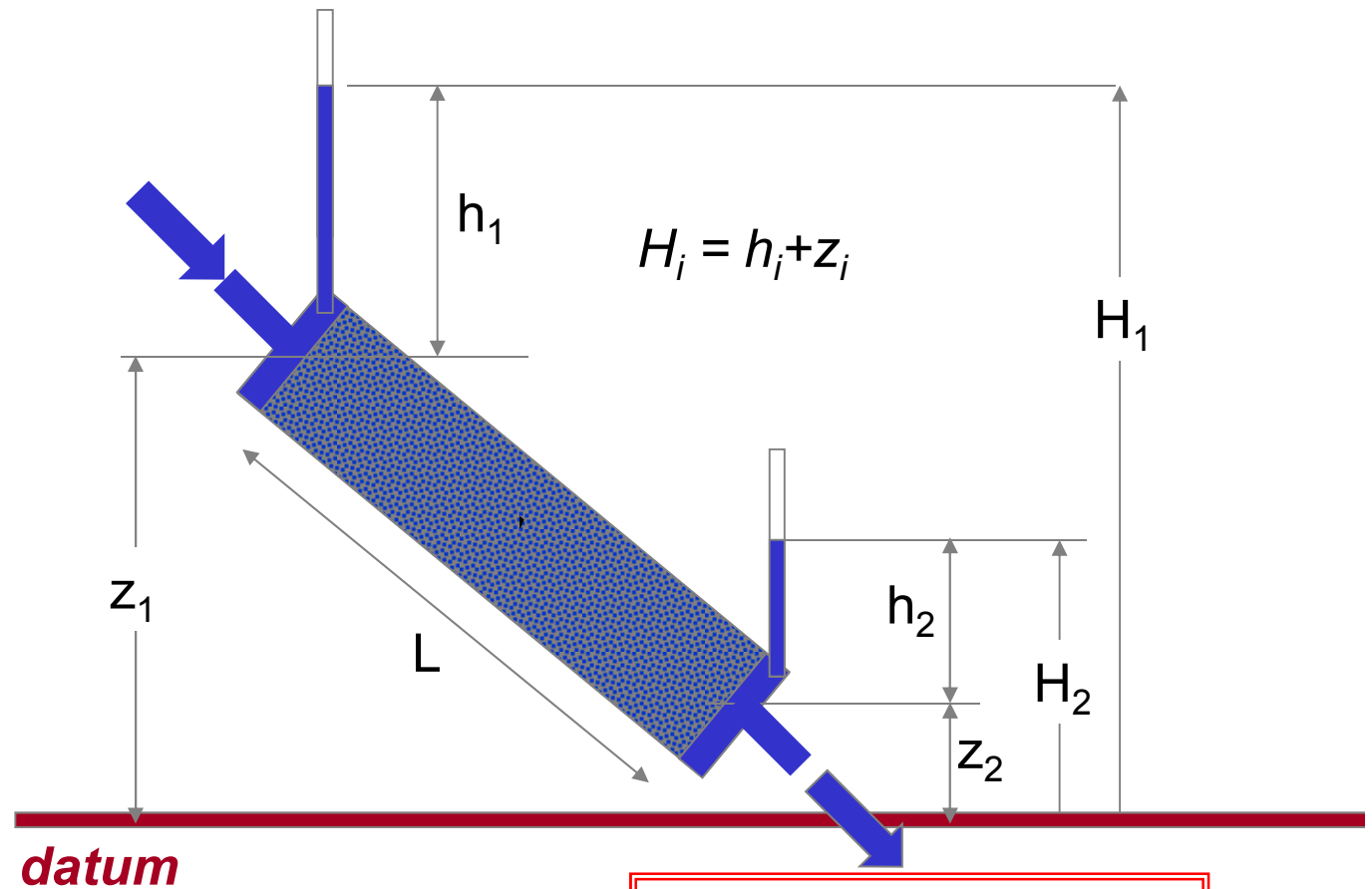


Darcy, H., 1856. *Les Fontaines de la Ville de Dijon*



# Darcy law

$$Q = \frac{K_s A \Delta H}{L}$$



$Q = \text{flow } [L^3 \cdot T^{-1}]$

$A = \text{crosssectional area } [L^2]$

$K_s = \text{saturated hydraulic conductivity } [L \cdot T^{-1}]$

$\Delta H = H_1 - H_2$  (hydraulic head drop)  $[L]$

$L = \text{sample length } [L]$

**valid in fully saturated porous media**  
**For example: under the ground water level**

for:

$$q = \frac{Q}{A}$$

kde:

$q$  ... Volume flux [ $L \cdot T^{-1}$ ]

$Q$  ... Flow rate [ $L^3 \cdot T^{-1}$ ]

$A$  ... Crosssectional area [ $L^2$ ]

Transforms to the:

$$q = K_s \frac{\Delta H}{L}$$

More general form:

$$q = K_s \frac{dH}{dl}$$

Pro 1D vertical flow

$$q = -K_s \frac{dH}{dl} = -K_s \nabla H$$

**poznámka: negative sign due to the fact grad  $H$  aims against flow direction**

# Coefficient or the saturated hydraulic conductivity $K_s$

*Also called (sometimes) filtration coefficient, darcy's coefficient or permeability (incorrect)*

commonly used units  $K_s$  ( $\text{m}\cdot\text{s}^{-1}$ ), ( $\text{cm}\cdot\text{d}^{-1}$ ), ( $\text{cm}\cdot\text{s}^{-1}$ )

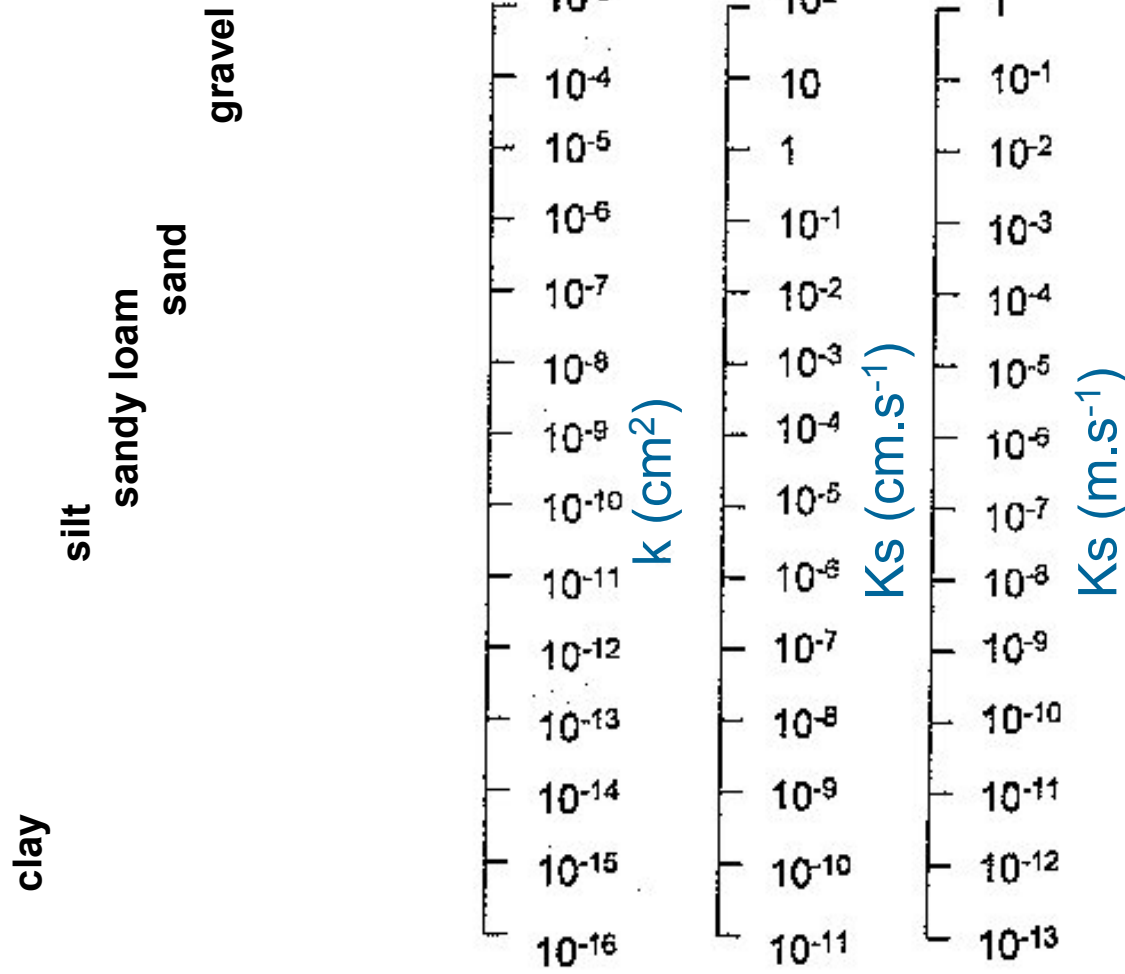
$K_s$  is property of water-solid interaction. Parameter which is related only to the porous media (independently on flowing liquid) is:

## Permeability $k$

$$k = K_s \nu / g \quad [L^2]$$

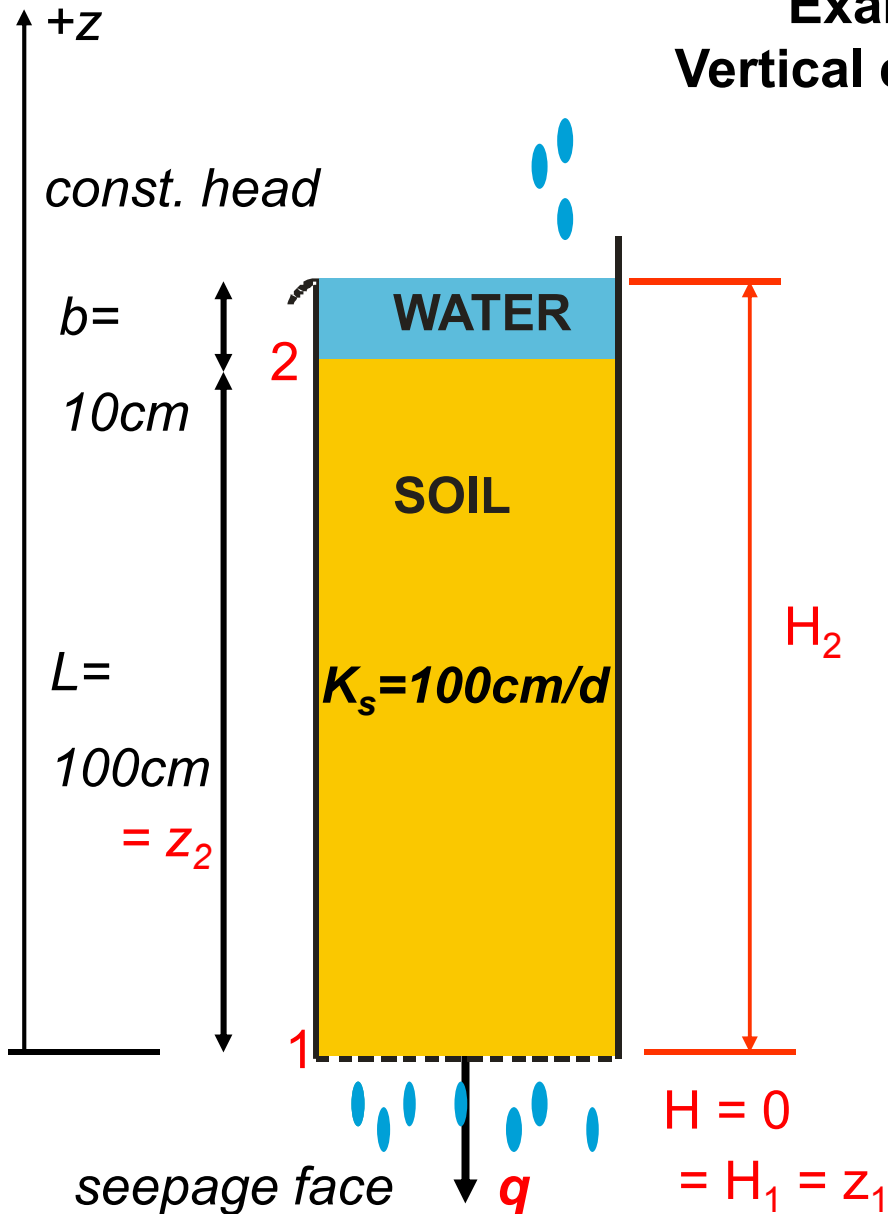
$k$  de  $\nu$  kinematic viscosity

# Ks for different media



### Example 1 :

Vertical column:  $q=?$



1) datum definition

2) points 1 and 2 with known hydraulic heads

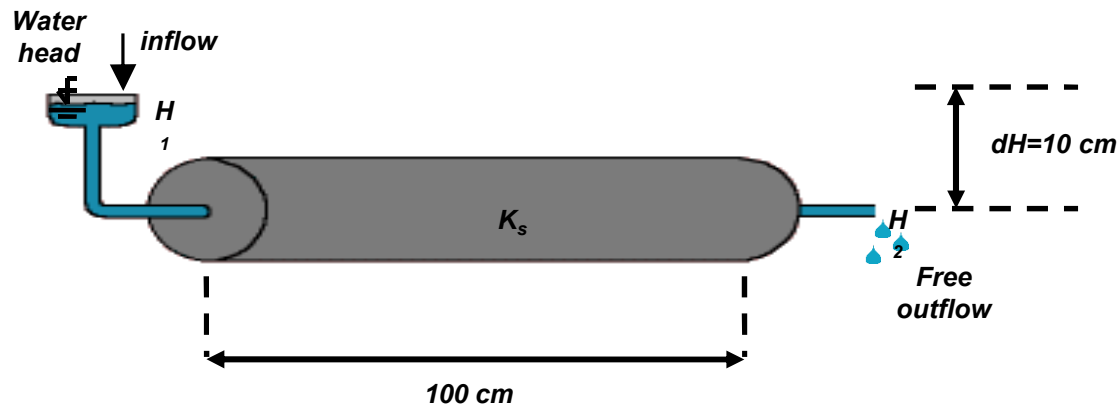
3) Darcy's law

$$q = -K_s \frac{\Delta H}{L} = -K_s \frac{(H_2 - H_1)}{L} =$$
$$= -100 \frac{(110 - 0)}{100} = -110 \text{ cm.d}^{-1}$$

## Example 2

### horizontal column: $q = ?$

1) Step 1, definition of datum and coordination system



2) Definition of points 1 and 2). Then  $x_1 = 0$  and  $h_1 = 10\text{ cm}$ ,  
 $x_2 = 100\text{ cm}$ ,  $h_2 = 0$ ,  $z_1 = z_2 = 0$ ,  $L = x_2 - x_1 = 100\text{ cm}$

3) Hydraulics heads are then  $H_1 = h_1 + z_1 = 10\text{ cm}$ ,  $H_2 = h_2 + z_2 = 0\text{ cm}$

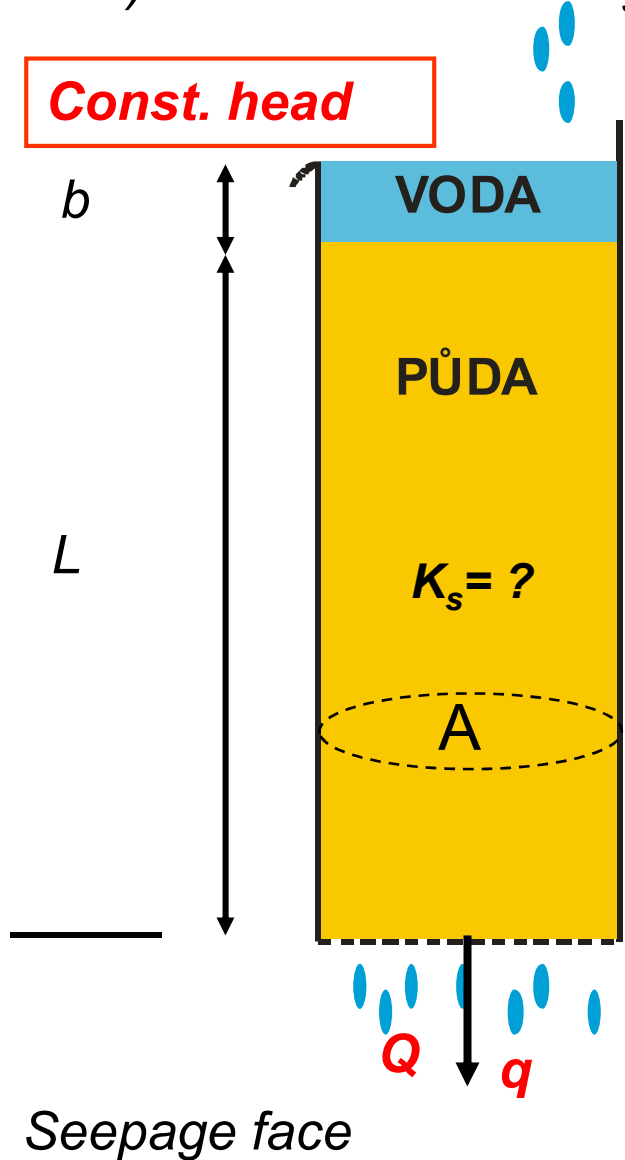
5) Darcy's law

$$q = -K_s \frac{\Delta H}{L} = -K_s \frac{(H_2 - H_1)}{L} = -100 \frac{(0 - 10)}{100} = 10\text{ cm.d}^{-1}$$



# $K_s$ measurements

1) Measurements of  $K_s$  using constant head permeameter



Soil column

$$H_1 = 0 + 0 \text{ (lower end)}$$

$$H_2 = b + L \text{ (upper end)}$$

$$\Delta H = (b+L) - 0$$

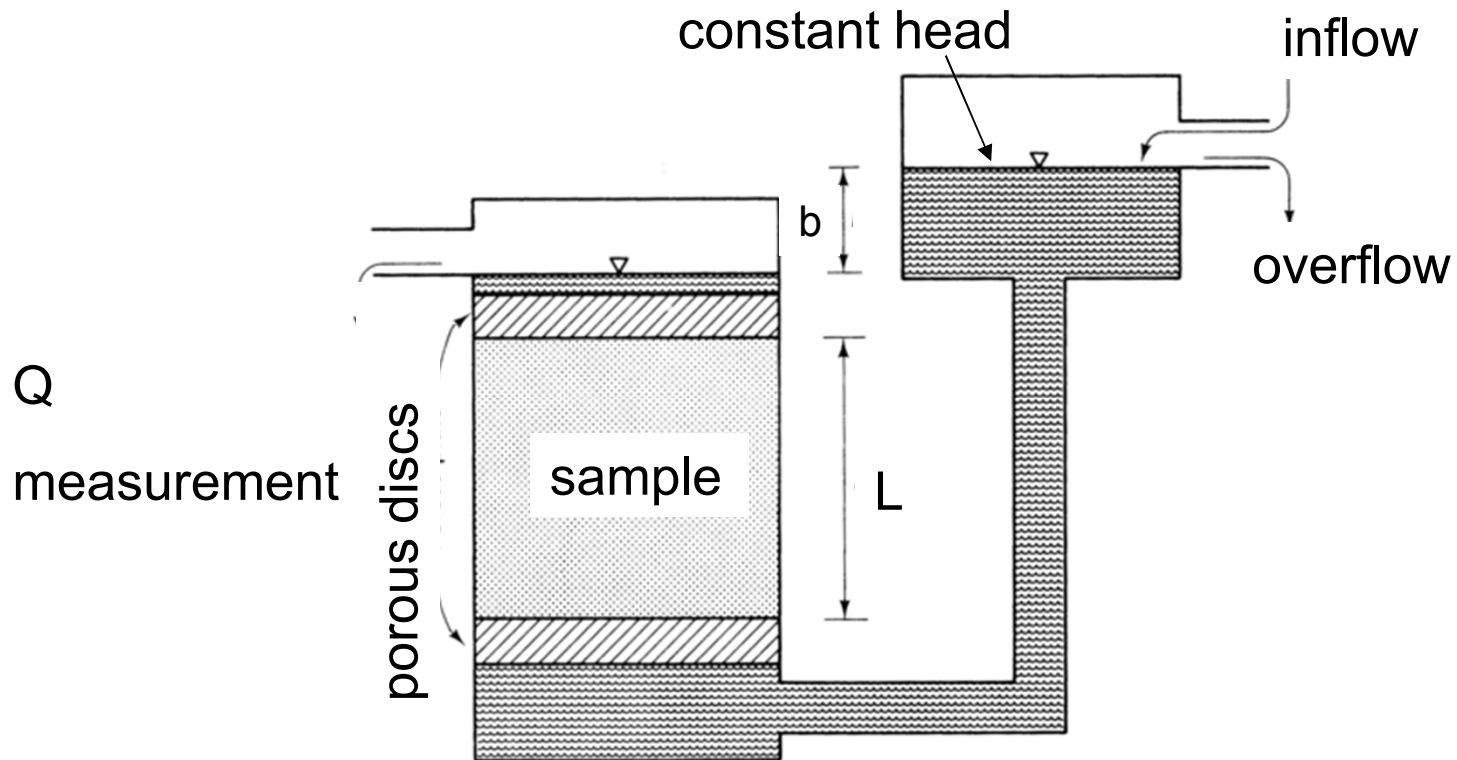
then:

$$K_s = -\frac{qL}{\Delta H} = -\frac{qL}{(b+L)}$$

In practice we measure  $Q$ , resp.  $V/t$ , then:

$$K_s = \frac{VL}{At\Delta H} = \frac{VL}{At(b+L)}$$

# Constant head permeameter

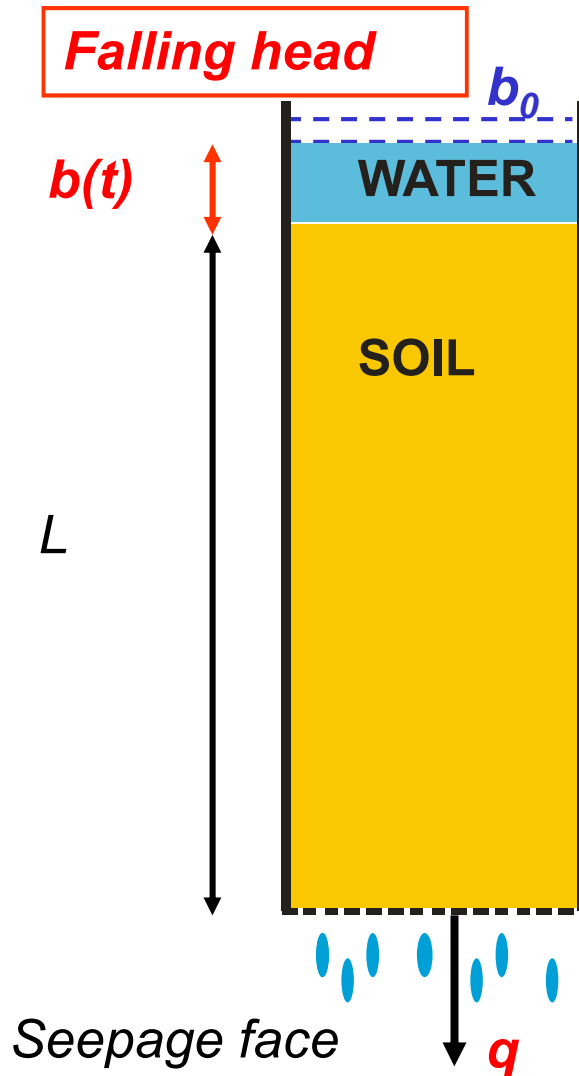


*soil sample must be carefully saturated with water to measure "real"  $K_s$ .*

# Constant head permeameter



## 2) Measurement of $K_s$ falling-head permeameter



Experiment is done on soil sample in the laboratory. Initial water level is equal to  $b_0$   
 $H_1 = 0, H_2(t) = L + b(t), \quad \Delta H(t) = [b(t) + L] - 0$

$$q = \frac{db}{dt} = -K_s \frac{(b + L)}{L} \quad \text{becomes:}$$

$$\frac{db}{b + L} = -\frac{K_s}{L} dt$$

Integration of the left side

$$\int_{b_0}^{b_1} \frac{db}{b + L} = \ln(b + L) \Big|_{b_0}^{b_1} = \ln \frac{b_1 + L}{b_0 + L}$$

*Right side integration*

$$-\int_0^{t_1} \frac{K_s}{L} dt = -\frac{K_s}{L} \int_0^{t_1} dt = -\frac{K_s t_1}{L} \qquad \frac{db}{b+L} = -\frac{K_s}{L} dt$$

*then:*

$$\ln \frac{b_1 + L}{b_0 + L} = -\frac{K_s t_1}{L}$$

$$K_s = \frac{L}{t_1} \ln \frac{b_0 + L}{b_1 + L}$$

# Falling-head permeameter

Consider different cross-sectional areas of burette and column:

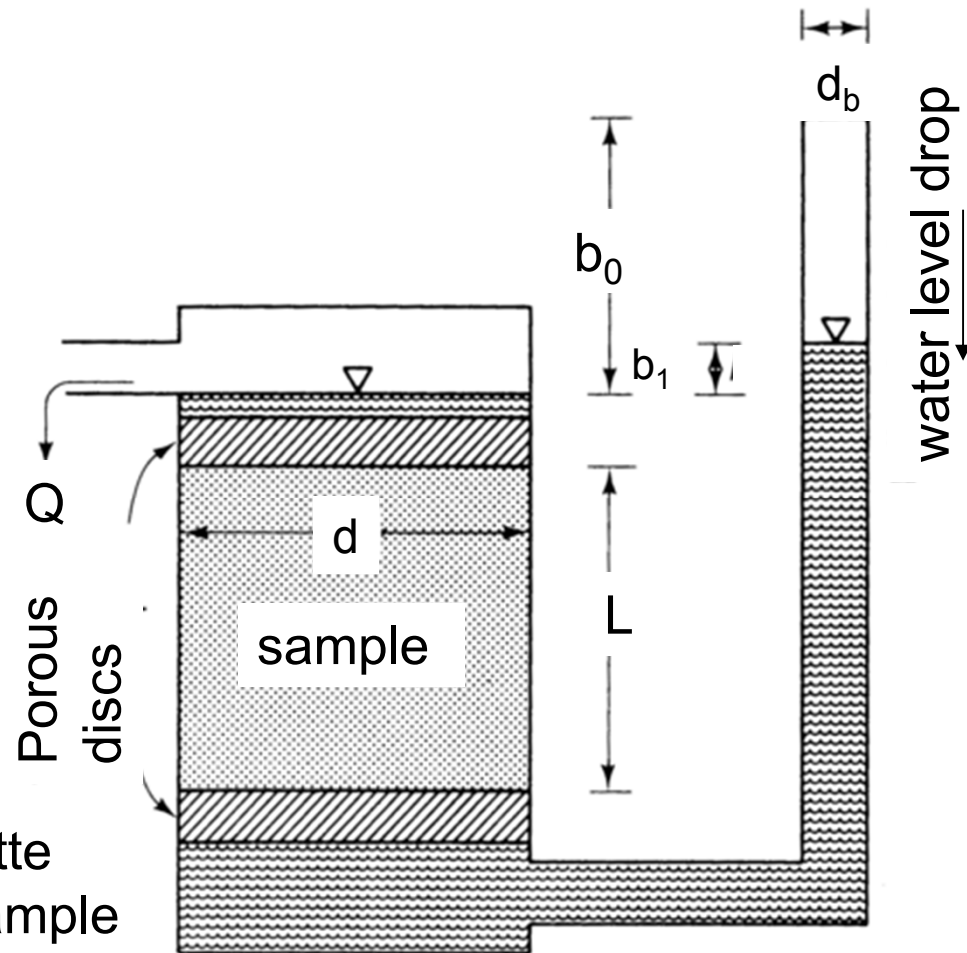
$$K_s = \frac{A_b L}{A t_1} \ln \frac{b_0 + L}{b_1 + L}$$

where:

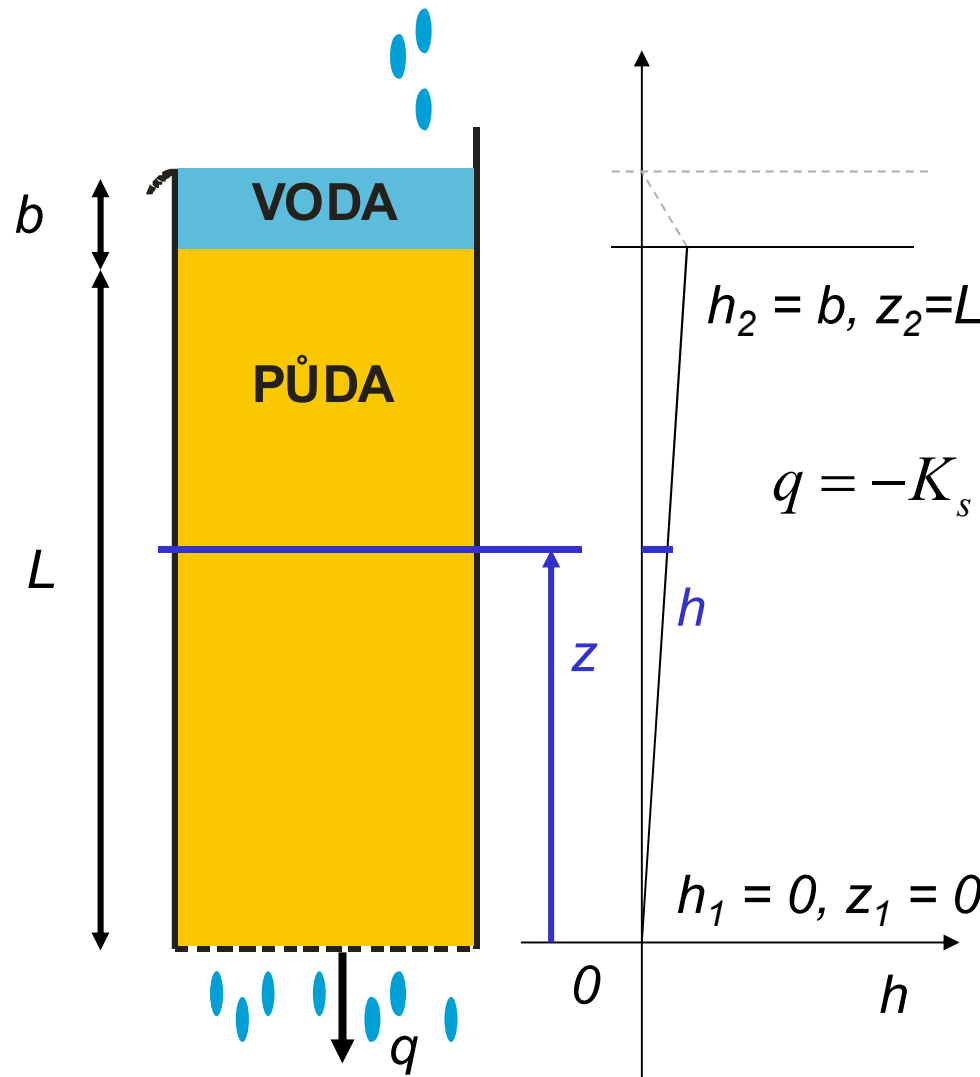
$t_1$  ... time

$A_b$  ... cross. area of burette

$A$  ... cross. area of the sample



**Example 3 :**  
**Pressure head along the soil column  $h(z)=?$**



$K_s$  is constant,  $h(z) = ?$

Darcy's law:

$$q = -K_s \frac{\Delta H}{L} = -K_s \frac{b + L}{L} = -K_s \frac{h + z}{z}$$

$$h = \frac{h_2 - h_1}{L} z = \frac{b}{L} z$$

In this case, pressure head profile is linear .



# Measurements of $K_s$ in field – infiltration experiments

Flux across the surface is called infiltration rate  $i$ .

Total amount of water infiltrated is  $I$  [L]

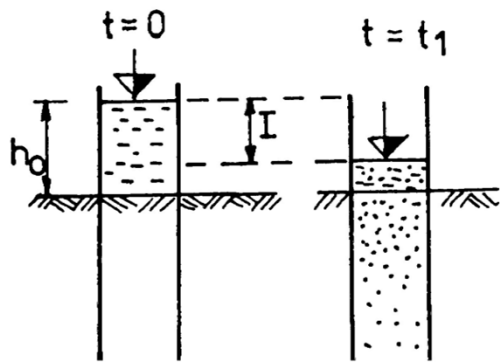
Infiltration rate can be steady or unsteady



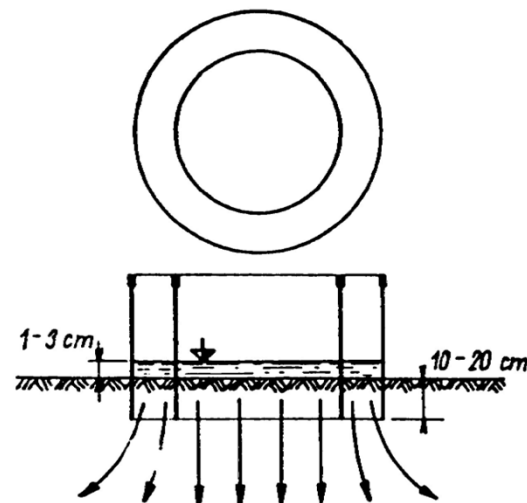


# Measurements of $K_s$ in field

Ideal case



Common practice

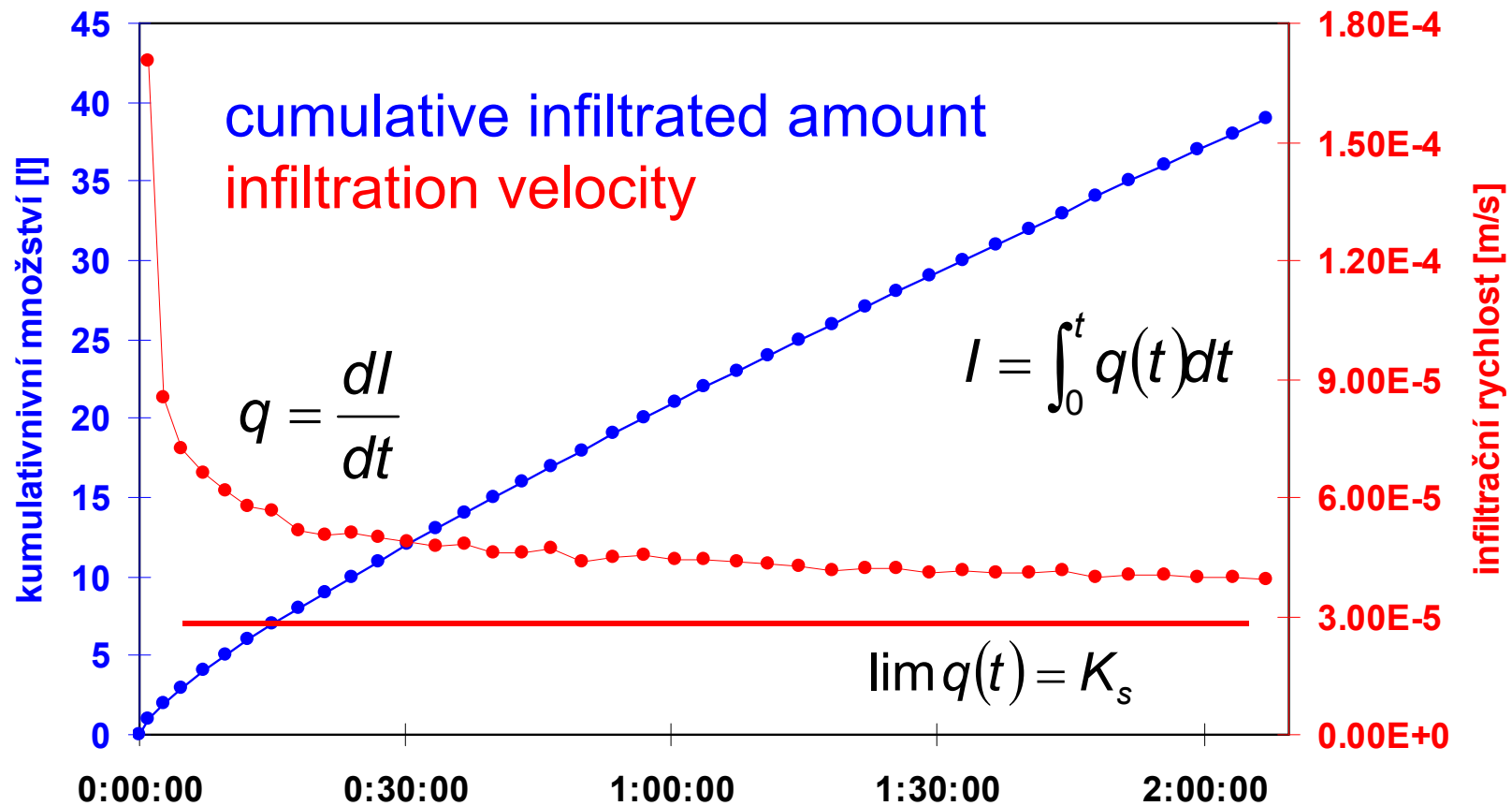


Double-ring infiltration:

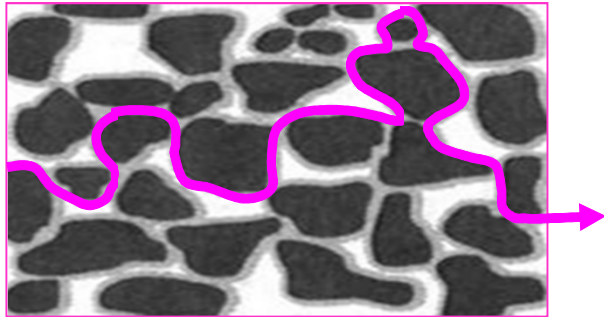
- Two rings
- Spike inserted inside of the inner ring
- water batches are being added to the inner ring, every time the water level reaches the spike
- The time between spike appearance is measured for each batch and flux is then calculated for each time interval



# Evaluation of double ring infiltration

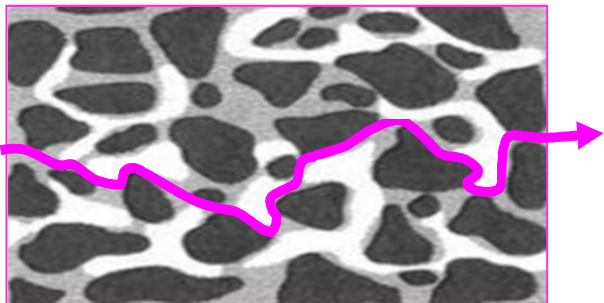


# Unsaturated hydraulic conductivity

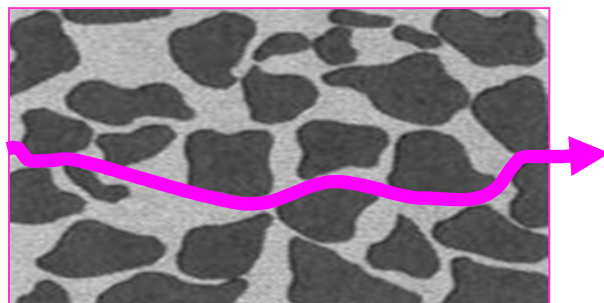


- $\theta$  changes in time and space

- relationship  $\theta(h)$  e.g. retention curve exist



- hydraulic conductivity **depends on  $\theta$**  resp. on  **$h$  for  $h < 0$**



- $K(\theta)$ , resp.  $K(h)$  is called hydraulic conductivity function

Zdroj: E. Sulzman

# Darcy-Buckingham law

Edgar Buckingham (1907)

$$q = -K(\theta)\nabla H$$

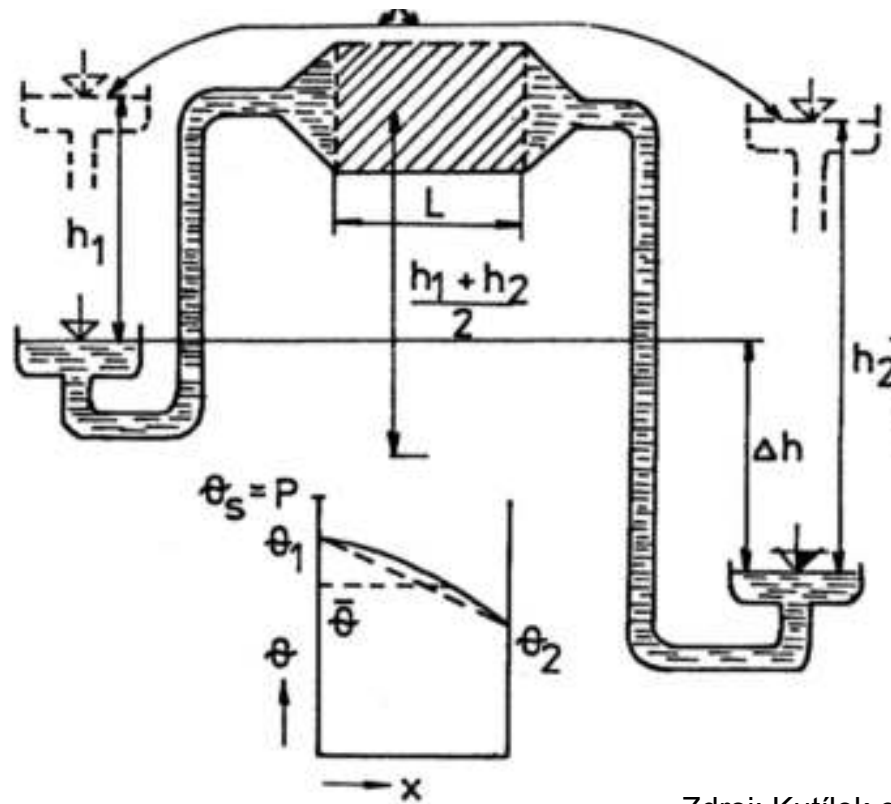
where:

$q$  flux

$H$  hydraulic head



flow direction at  $dh$   
original level



Zdroj: Kutílek et al. 1994

# Capillary models

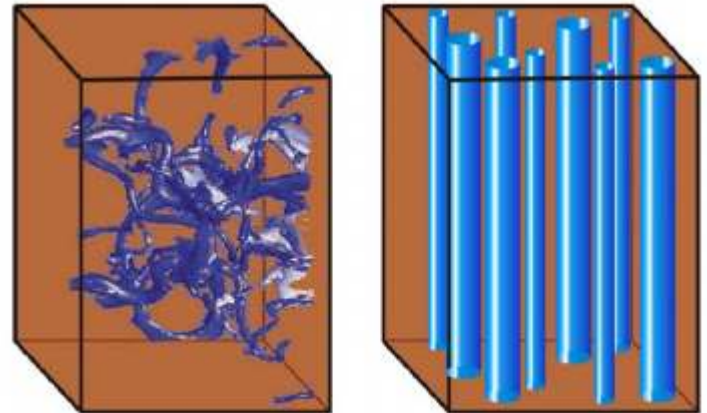
## *Capillary models (Childs and Collis-George, 1950)*

Based on assumption that from known of pore size distribution (from retention curve) and equation and Laplace equation, and Equation describing the flow in individual capillary the unsaturated Hydraulic conductivity can be predicted

Capillary models predict relative hydraulic conductivity

$$K(\theta) = K_r(\theta)K_s$$

where  $K_s$  is measured saturated hydraulic conductivity



# Relative hydraulic conductivity

We will obtain the hydraulic conductivity of the capillary model as follows:

$$K(\theta) = C_1^2 C_2 \int_0^\theta \frac{1}{h^2} d\theta$$

Then for relative hydraulic conductivity  $K_r$

$$K_r(\theta) = \frac{K(\theta)}{K(\theta_s)} = \frac{\int_0^\theta \frac{d\theta}{h^2}}{\int_0^{\theta_s} \frac{d\theta}{h^2}}$$

**constants  $C_1^2$  a  $C_2$  are canceled**

where:  $K(\theta_s) = K_s$  Is saturated hydraulic conductivity

# Most commonly used models of Kr prediction

$(\theta/\theta_s)^b$  ..... Relative tortuosity is included

**Burdine (1953):**

$$K_r(\theta) = \left(\frac{\theta}{\theta_s}\right)^2 \frac{\int_0^\theta \frac{d\theta}{h^2}}{\int_0^{\theta_s} \frac{d\theta}{h^2}}$$

$$\theta_e(h) = \begin{cases} \left(\frac{H_b}{h}\right)^\lambda & h < H_b \\ 1 & h \geq H_b \end{cases}$$

Brooks a Corey

Retention curves functions are substituted.....

**Mualem (1976):**

$$K_r(\theta) = \left(\frac{\theta}{\theta_s}\right)^{1/2} \left[ \frac{\int_0^\theta \frac{d\theta}{h}}{\int_0^{\theta_s} \frac{d\theta}{h}} \right]^2$$

$$\theta_e(h) = \begin{cases} \frac{1}{(1 + (-\alpha h)^n)^m} & h < 0 \\ 1 & h \geq 0 \end{cases}$$

van Genuchten

## ..... and the final expressions for Kr predictions are then

From Brooks and Corey  $K_r(\theta_e) = \theta_e^{b+a\lambda}$

$$K_r(h) = \begin{cases} \left(\frac{H_b}{h}\right)^{a+b/\lambda} & h < H_b \\ 1 & h \geq H_b \end{cases}$$

Where parameters a and b are for Burdine model Burdine a=2 a b=3  
Mualem a=2 a b=2.5

$$\theta_e = \frac{\theta - \theta_r}{\theta_s - \theta_r} \quad \text{Effective water content}$$



.....

from van Genuchten  
vztahu

$$K_r(\theta_e) = \theta_e^{0.5} [1 - (1 - \theta_e^{\frac{1}{m}})^m]^2$$

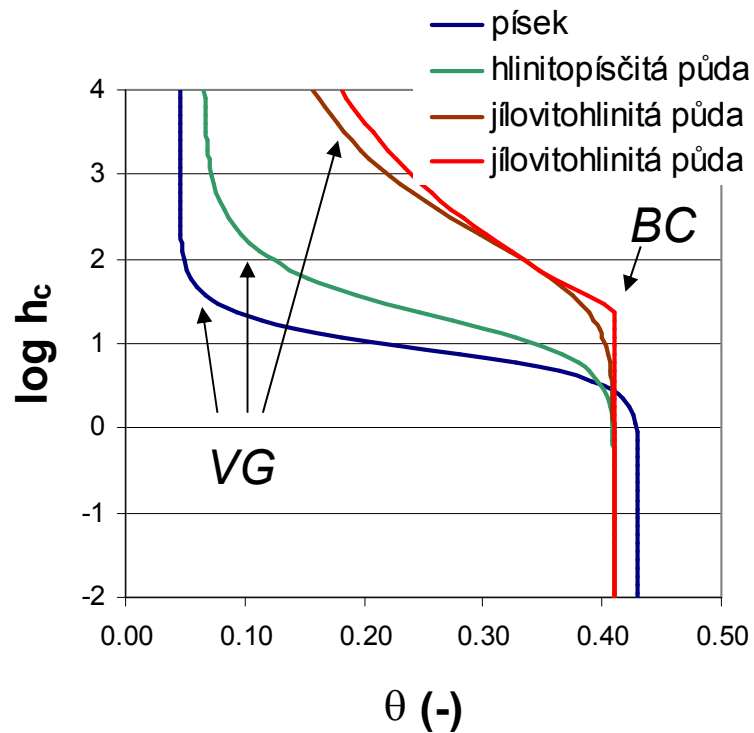
$$\theta_e = \frac{\theta - \theta_r}{\theta_s - \theta_r}$$

$$K_r(h) = \begin{cases} \frac{\left\{ 1 - (-\alpha h)^{mn} [1 + (-\alpha h)^n]^{-m} \right\}^2}{[1 + (-\alpha h)^n]^{m/2}} & h < 0 \\ 1 & h \geq 0 \end{cases}$$

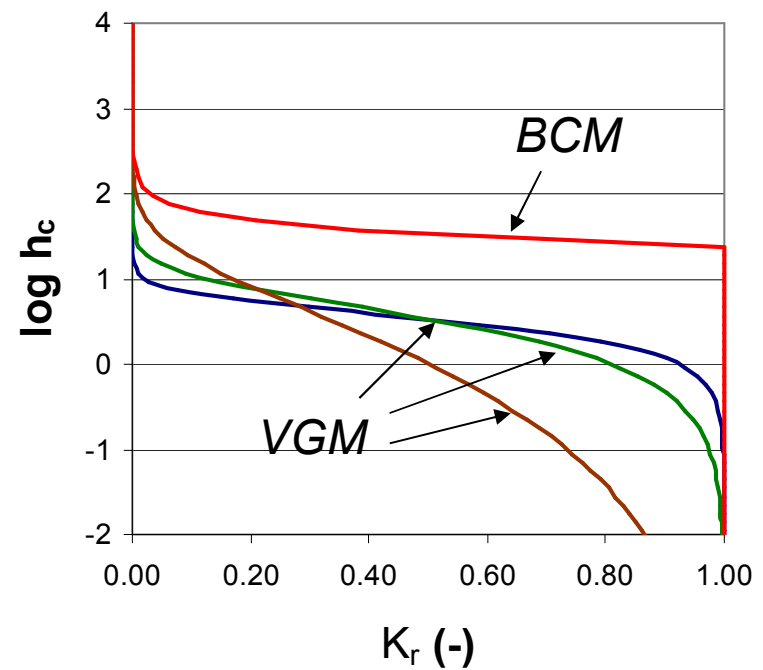
Mualem

# Retention curve and hydraulic conductivity function for different soils

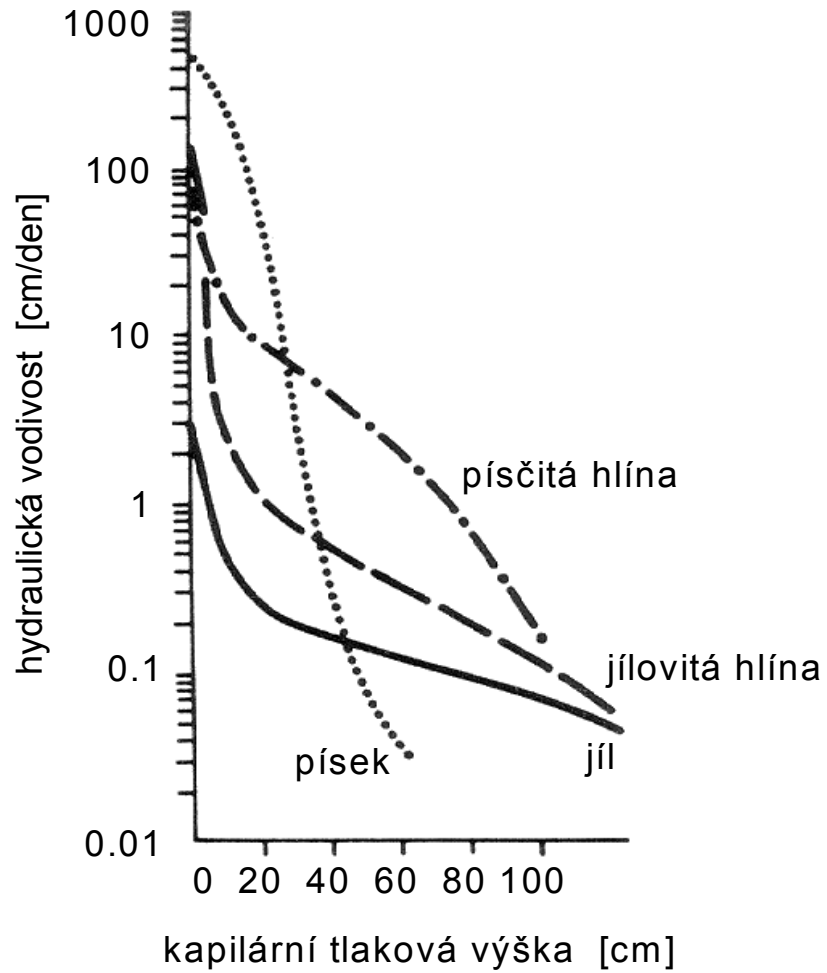
*Retention curve*



*Hydraulic conductivity function*



# Unsaturated hydraulic conductivity



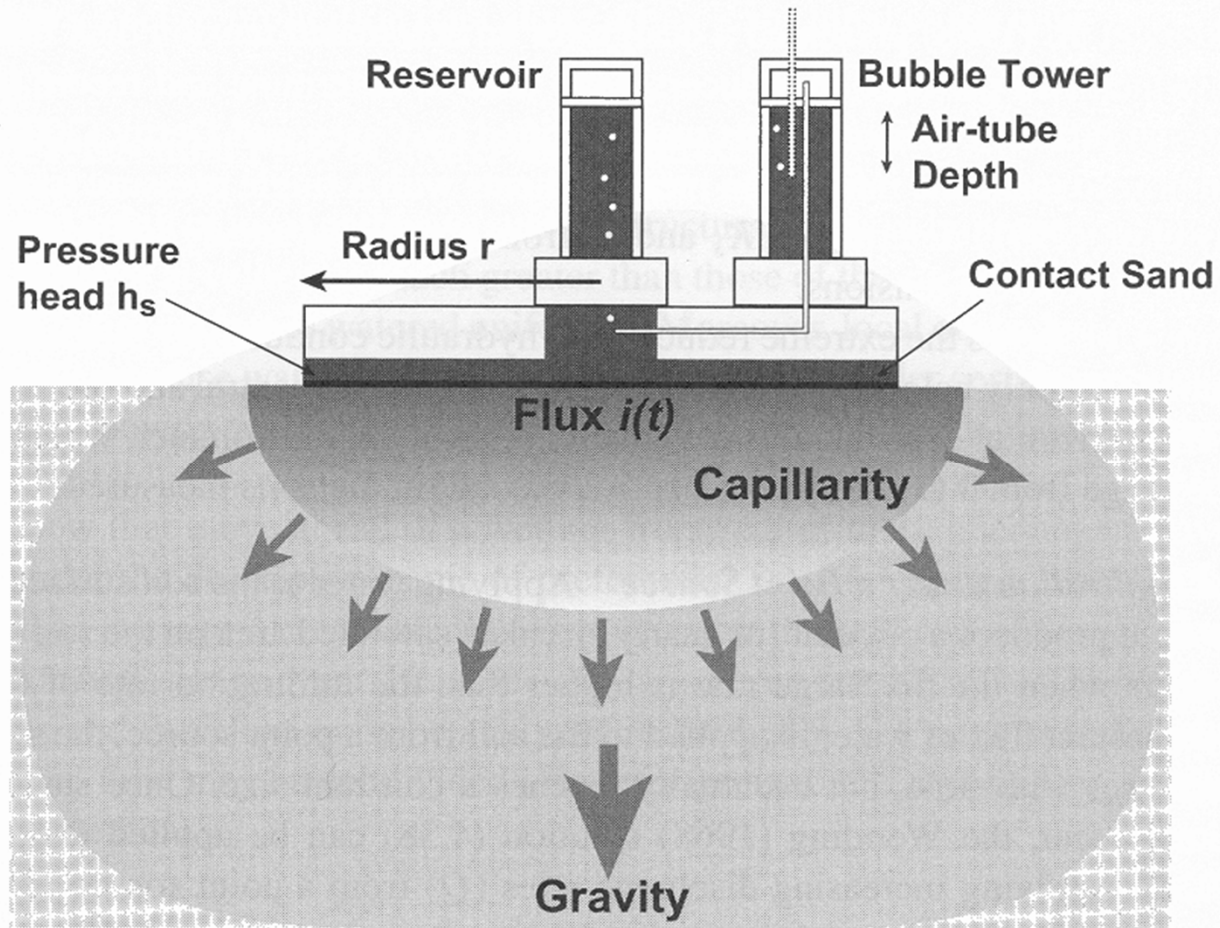
# Measurements of hydraulic conductivity in field



## ***Tension infiltrometer***

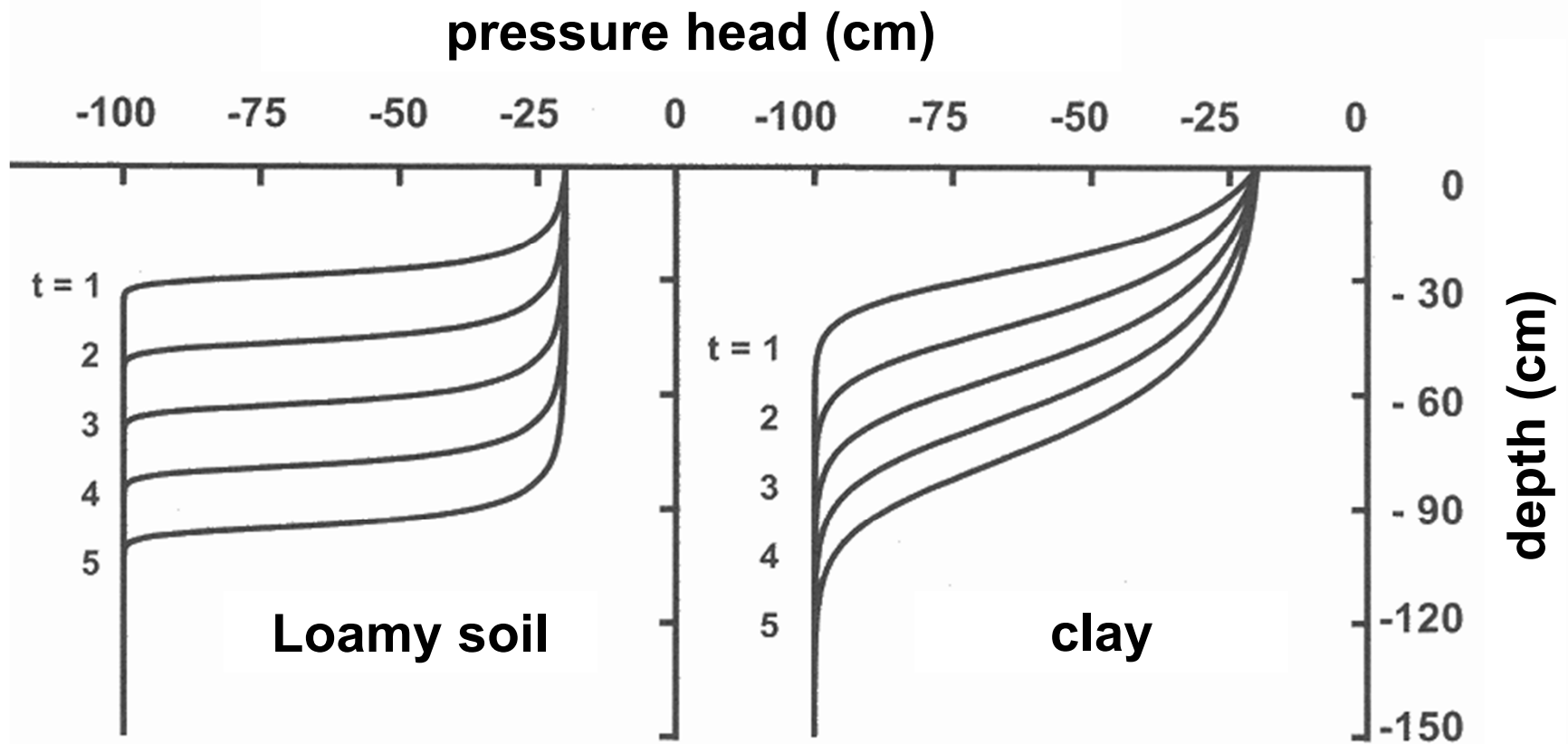
*Measurements of  $I$  under  
infiltrometer with fixed  
tension head*

# Tension infiltrometer



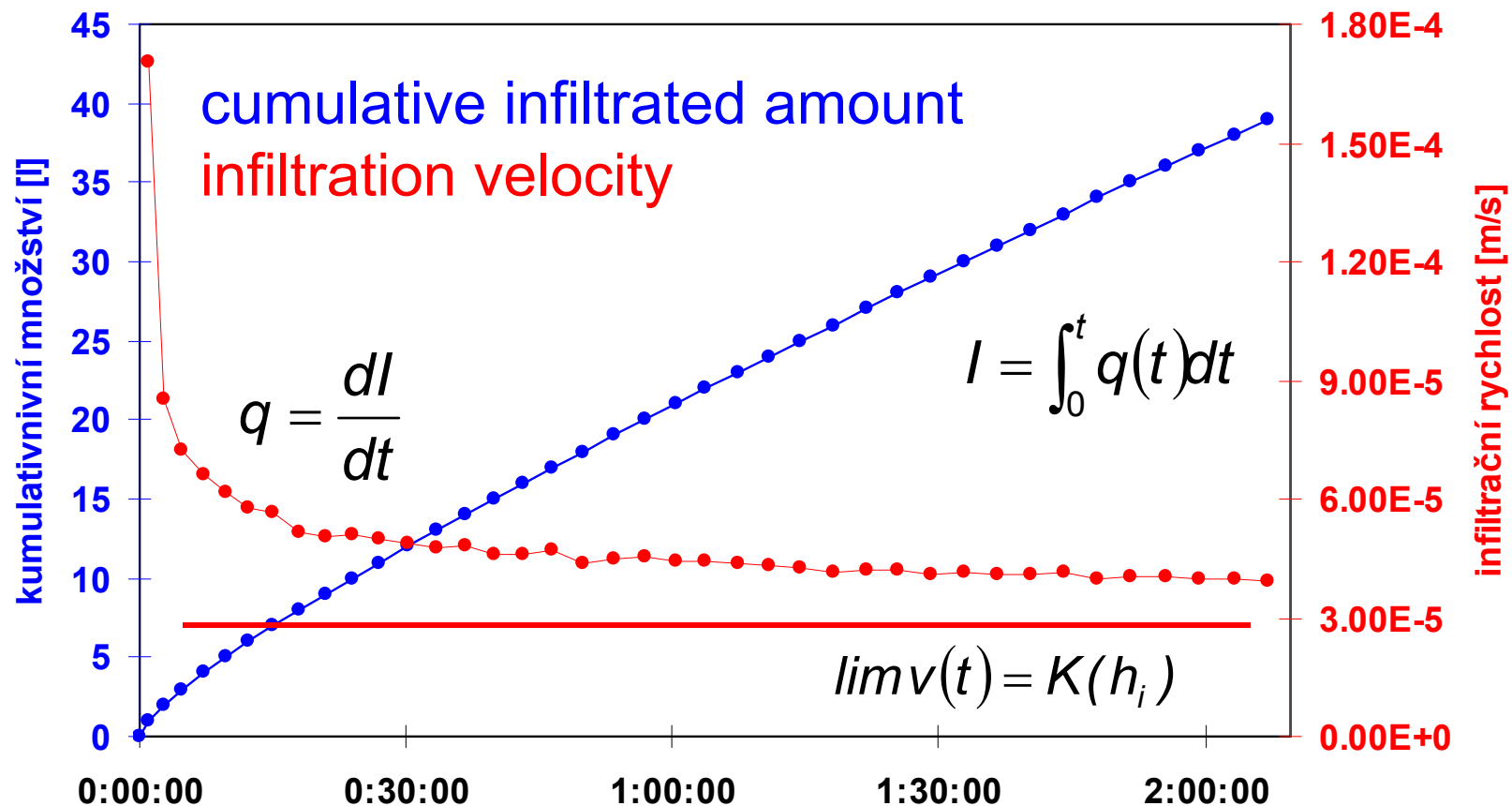
Jury a Horton 2004

# Infiltration experiment – the wetting front



# Result of one infiltration experiment

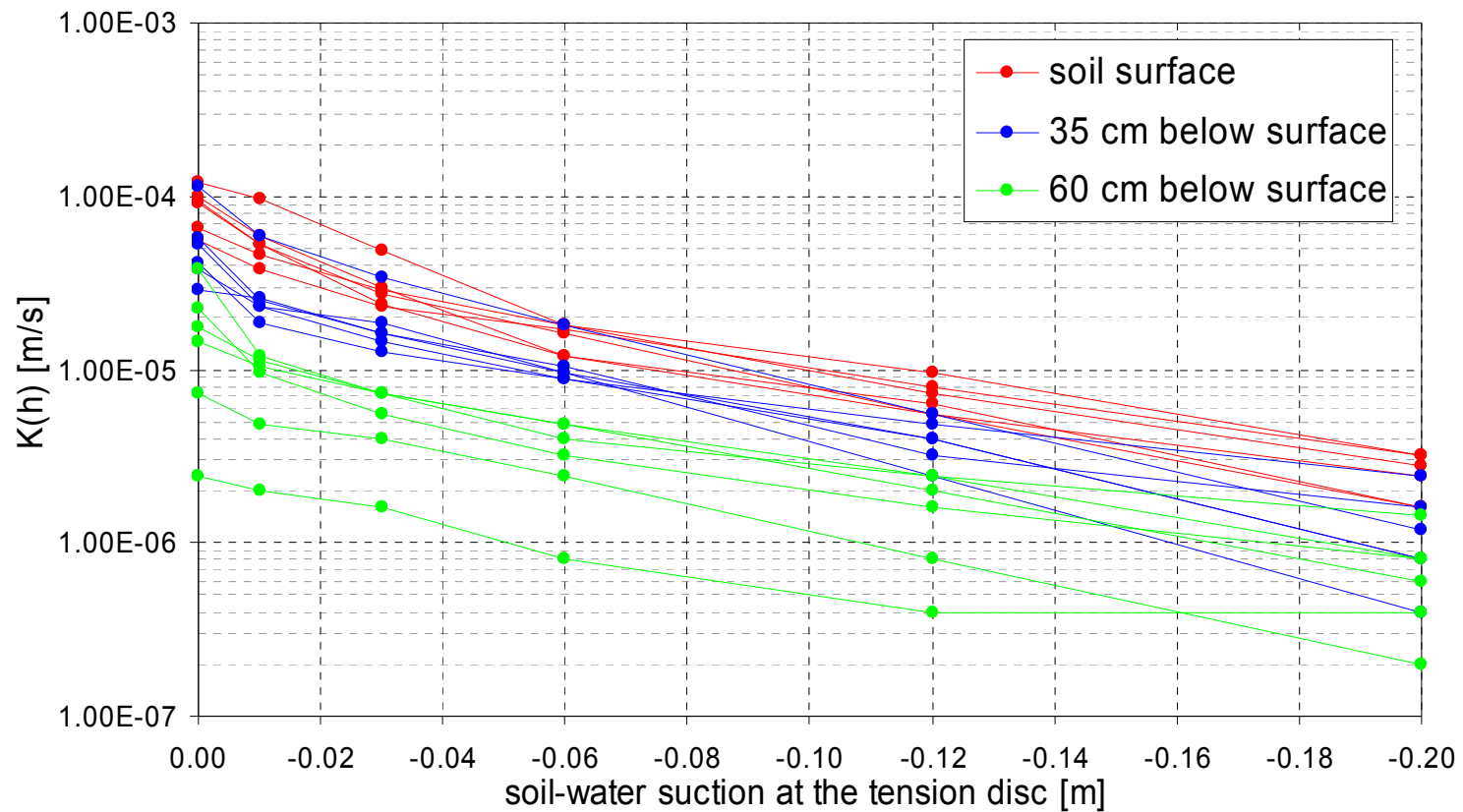
- analogous to  $K_s$
- One  $K(h_i)$  value for each infiltration done with the pressure head  $h_i$





# Measurement of $K(h)$ in field

- Clay loam soil

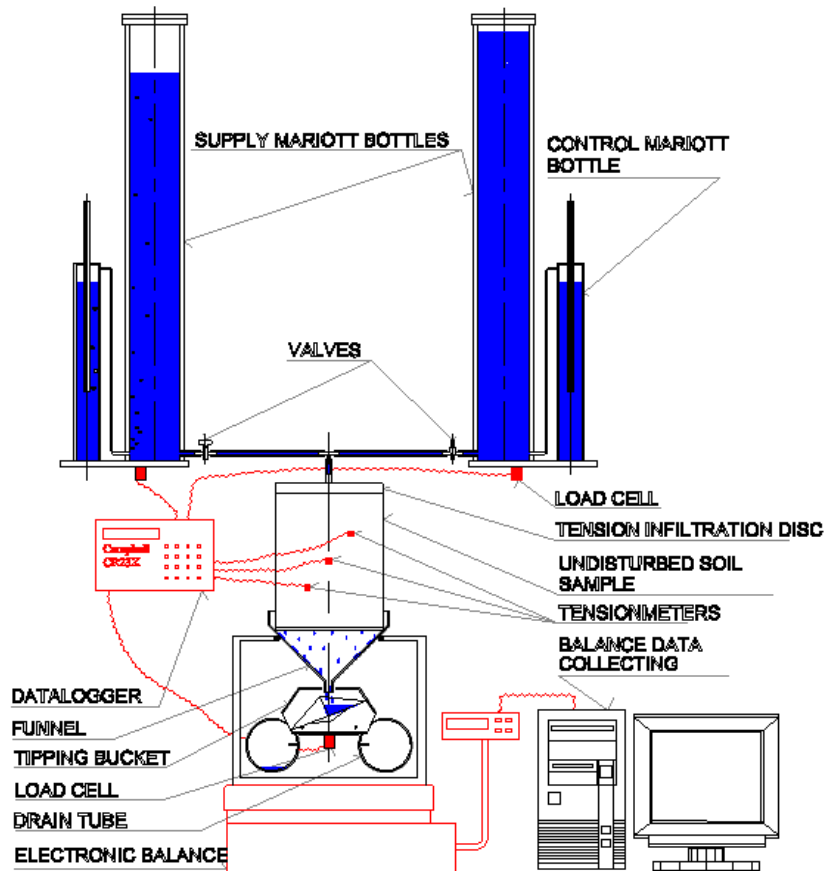




# Measurements of $K(h)$ in laboratory

- evaluation using inverse modeling

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# References

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